Advantages and Disadvantages of Different Types of Neutral Grounding Systems

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NEUTRAL GROUNDING OF POWER SYSTEMS

OBJECTIVES

1. Discuss five types of grounding for power systems.
2. Discuss advantages of high resistance grounding.
3. Show equipment
POWER SYSTEM GROUNDING

Power system grounding is a connection between an electrical circuit or equipment and the earth or to some conducting body that serves in place of earth.

This presentation concerns the design of power system grounding for industrial and commercial facilities – not utility systems.
DISCUSSION OF GROUNDING

1. Ungrounded system
2. Solidly grounded system
3. Reactive grounded system
4. Low resistance grounded system
5. High resistance grounded system
Are You at Risk?

Do you use electricity?

Electrical deficiencies are the leading ignition source and cause of fire and explosion.
What is a Ground Fault?

Contact between ground and an energized conductor

Unleashes large amount of electrical energy

Dangerous to equipment and people
### POWER SYSTEM GROUNDING

#### SYSTEM FAILURES – SHORT CIRCUITS (FAULTS)

**INDUSTRIAL POWER SYSTEMS**

<table>
<thead>
<tr>
<th>FAILURE MODE</th>
<th>PERCENTAGE OF FAILURES</th>
</tr>
</thead>
<tbody>
<tr>
<td>LINE TO GROUND</td>
<td>98 %</td>
</tr>
<tr>
<td>PHASE - PHASE</td>
<td>&lt;1.5 %</td>
</tr>
<tr>
<td>THREE PHASE</td>
<td>&lt;.5 %</td>
</tr>
</tbody>
</table>

Most three phase faults are man-made:

I.E. Accidents caused by improper operating procedure.
Two Types of Faults

Bolted Faults
Solid connection between two phases or phase and ground resulting in high fault current.
Stresses are well contained so fault creates less destruction.

Arc Faults
Usually caused by insulation breakdown, creating an arc between two phases or phase to ground.
Intense energy is not well contained, and can be very destructive.
600 Volt “THHN” Power Cable on “Ungrounded” System

Arcing Fault
Arc Fault

Usually caused by insulation breakdown, an arc jumps between two phases or between one phase and a grounded metal surface.

The resulting fault current is smaller because of the relatively high resistance of the arc (25-40% of a bolted fault).

Protective devices may be slow in responding to the smaller fault current.

Arc faults can be the most destructive because of the intense energy that is concentrated in the small area of the arc.

The majority of the stresses (thermal and mechanical) are not confined within the busbar and associated supports, it extends to the space in the compartment.
An arcing fault is an intermittent failure between phases or phase to ground. It is a discontinuous current that alternately strikes, is extinguished and restrikes again. For solidly grounded systems, the arc currents are: in percent of bolted three phase faulted

<table>
<thead>
<tr>
<th>Faults</th>
<th>Percentage</th>
</tr>
</thead>
<tbody>
<tr>
<td>THREE PHASE</td>
<td>89%</td>
</tr>
<tr>
<td>LINE-LINE</td>
<td>74%</td>
</tr>
<tr>
<td>LINE-GROUND</td>
<td>38%</td>
</tr>
</tbody>
</table>
ARCING LINE-GROUND POWER SYSTEM

ARCING GROUND FAULT CURRENT

$e_{peak} = 390V$
$e_{gap} = 375V$
$e_{arc} = 140V$
$I_{RMS} = 7600A$

FROM: THE IMPACT OF ARCING GROUND FAULTS ON LOW VOLTAGE POWER SYSTEM DESIGN J.R. DUNKLE-JACOBS GET-6098 12-T0 PG.19 FIG 4-2 GENERAL ELECTRIC

Note: Current is a discontinuous, non-sinusoidal wave
Arcing Ground Faults
Intermittent or Re-strike

**Intermittent ground fault:** A re-striking ground fault can create a high frequency oscillator (RLC circuit), independent of L and C values, causing high transient over-voltages.

- i.e. re-striking due to ac voltage waveform or loose wire caused by vibration
Arcing Ground Faults
Intermittent or Re-strike

Plot of transient over-voltage for an arcing ground fault
8.2.5 If this ground fault is intermittent or allowed to continue, the system could be subjected to possible severe over-voltages to ground, which can be as high as six to eight times phase voltage. Such over-voltages can puncture insulation and result in additional ground faults. These over-voltages are caused by repetitive charging of the system capacitance or by resonance between the system capacitance and the inductance of equipment in the system.
THE UNGROUNDED POWER SYSTEM
THE UNGROUNDED POWER SYSTEM

DELTA - DELTA CONNECTION

SINGLE PHASE LOAD

SUITABLE FOR

TWO WIRE, SINGLE PHASE LOADS
THREE WIRE, THREE PHASE LOADS
UNGROUNDED SYSTEM
NORMAL CONDITIONS

2000 KVA, 480 VOLT SYSTEM

\[ |I_g| = |I_{ca}| = |I_{cb}| + |I_{cc}| = 0 \]
\[ X_{co} = 277 \text{ OHMS (TYPICAL)} \]
UNGROUNDED SYSTEM
NORMAL CONDITIONS

VECTORS FOR NORMAL OPERATION

- BALANCED CONDITIONS
- CURRENTS DISPLACED 120 DEGREES
- CAPACITOR NEUTRAL AT SAME POTENTIAL AS TRANSFORMER NEUTRAL
- CAPACITOR CURRENT LEADS CAPACITOR VOLTAGE BY 90 DEGREES

$V_a = 277$ VOLTS
UNGROUNDED SYSTEM
GROUND FAULT ON PHASE A

VOLTAGES ACROSS $X_{co}$ INCREASE BY 1.73
CAPACITORS CURRENTS NOW 60 DEG. APART

$I_c = 1.73A$

$I_g = 3.0A$

$I_{cb} = 1.73A$
UNGROUNDED SYSTEM
GROUND FAULT ON PHASE A
THE UNGROUNDED POWER SYSTEM
GROUND DETECTION CIRCUIT

MAIN BUS

φC

φB

φA

ON

ON

ON

3-PT’S

SYSTEM NORMAL
ALL LIGHTS ON WITH EQUAL BRIGHTNESS
THE UNGROUNDED POWER SYSTEM
GROUND DETECTION CIRCUIT

GROUND FAULT ON PHASE A
PHASE A LIGHT OUT
PHASE B & PHASE C LIGHTS ON AT GREATER BRIGHTNESS - i.e., VOLTAGE ON THE LIGHTS HAS INCREASED BY 73%
THE UNGROUNDED POWER SYSTEM

ADVANTAGES

1. Low value of current flow for line to ground fault - 5 amps or less.
2. No flash hazard to personnel for accidental line to ground fault.
3. Continued operation on the occurrence of first line to ground fault.
4. Probability of line to ground arcing fault escalating to line – line or three phase fault is very small.
THE UNGROUNDED POWER SYSTEM

DISADVANTAGES

1. Difficult to locate phase to ground fault.
2. The ungrounded system does not control transient overvoltages.
3. Cost of system maintenance is higher due to labor of locating ground faults.
4. A second ground fault on another phase will result in a phase-phase short circuit.
THE SOLIDLY GROUNDED POWER SYSTEM
THE SOLIDLY GROUNDED POWER SYSTEM

CONNECTION

A
B
M
C

LOAD

SUITABLE FOR
- TWO WIRE, SINGLE PHASE LOADS (LINE-LINE)
- TWO WIRE, SINGLE PHASE LOADS (LINE-NEUTRAL)
- THREE PHASE, THREE WIRE LOADS
SOLIDLY GROUNDED SYSTEM
THREE PHASE SHORT CIRCUIT

1500 KVA
13.8 KV - 480 VOLT
Z = 6.00%
SOLIDLY GROUNDED SYSTEM
THREE PHASE SHORT CIRCUIT

\[
IFL = \frac{1500 \text{ KVA}}{3 \times .48 \text{ KV}} = 1804 \text{ AMPS} = 1 \text{ PER UNIT}
\]

\[
I-3PH = \frac{E \text{ L-N}}{ZT} \times \frac{1.0 \text{ PER UNIT}}{.06 \text{ PER UNIT}} = 16.67 \text{ P.U.}
\]

\[
I3\phi = 16.67 \times 1804
\]

\[
I3\phi = 30,065 \text{ AMPS}
\]
SOLIDLY GROUNDED SYSTEM
LINE – GROUND SHORT CIRCUIT

\[ I = \frac{E_{L-N}}{Z_T + Z_G} = \frac{1.0}{0.06 + 0.02} = 12.5 \text{ PER UNIT} \]

\[ ILG = 12.5 \times 1804 = 22,550 \]
SOLIDLY GROUNDED SYSTEM
LINE – GROUND SHORT CIRCUIT

I PRIMARY = I SEC × \frac{V_s/\sqrt{3}}{V_P} 
= 22,250 \times \frac{480/\sqrt{3}}{13,800} 

I PRIMARY = 447 AMPS

THE LINE-GROUND FAILURE ON THE SECONDARY HAS CAUSED A SIGNIFICANT PROBLEM ON THE PRIMARY OF THE SYSTEM.
SOLIDLY GROUNDED SYSTEM
LINE-LINE SHORT CIRCUIT

\[
IL-L = \frac{E_{L-L}}{2XT} = \frac{EL-N \times \sqrt{3}}{2 \times T} = \frac{\sqrt{3}}{2} \frac{EL-N}{XT}
\]

\[
IL-L = 0.877 I \ 3 \ \varphi
\]

\[
IL-L = 0.877 I \ 3\phi
\]

IL-L = 26,367 AMPS
THE SOLIDLY GROUNDED POWER SYSTEM
LINE TO GROUND FAULT

I \text{ FAULT} \quad 500 \text{MVA SHORT CIRCUIT CAPACITY}
UTILITY POWER SYSTEM

<table>
<thead>
<tr>
<th>TRANSFORMER SIZE</th>
<th>I \text{ FAULT} @ 480 VOLT BUS</th>
<th>I \text{ FAULT} @ MOTOR</th>
</tr>
</thead>
<tbody>
<tr>
<td>1000KVA</td>
<td>20,000 AMPS</td>
<td>10,000 AMPS</td>
</tr>
<tr>
<td>1500KVA</td>
<td>30,000 AMPS</td>
<td>15,000 AMPS</td>
</tr>
<tr>
<td>2000KVA</td>
<td>40,000 AMPS</td>
<td>20,000 AMPS</td>
</tr>
</tbody>
</table>
Industry Recommendations

IEEE Std 141-1993 (Red Book)
Recommended Practice for Electric Power Distribution for Industrial Plants

7.2.4 The solidly grounded system has the highest probability of escalating into a phase-to-phase or three-phase arcing fault, particularly for the 480V and 600V systems. The danger of sustained arcing for phase-to-ground fault probability is also high for the 480V and 600V systems, and low for the 208V systems. For this reason ground fault protection is shall be required for system 1000A or more (NEC 230.95). A safety hazard exists for solidly grounded systems from the severe flash, arc burning, and blast hazard from any phase-to-ground fault.
THE SOLIDLY GROUNDED POWER SYSTEM

ADVANTAGES

1. Controls transient over voltage between the neutral and ground.
2. Not difficult to locate the fault.
3. Can be used to supply line-neutral loads
THE SOLIDLY GROUNDED POWER SYSTEM

DISADVANTAGES

1. Severe flash hazard
2. Main breaker may be required
3. Loss of production
4. Equipment damage
5. High values of fault current
6. Single-phase fault escalation into 3 phase fault is likely
7. Creates problems on the primary system
NEUTRAL GROUNDING RESISTOR
NEUTRAL GROUNDING RESISTOR with Transformer
Reactive Grounding

Uses reactor not resistor

Fault values of transient-overvoltages are unacceptable in industrial environments

Typically found in high voltage applications (>46 kV)
LOW RESISTANCE GROUNDING OF POWER SYSTEMS
LOW RESISTANCE GROUNDING OF POWER SYSTEMS

This design is generally for the following systems:

• At 2.4 kv through 25 kv.
• Systems serving motor loads
• Current is limited to 200 to 400 amps
• Systems typically designed to shut down in 10 seconds
LOW RESISTANCE GROUNDED POWER SYSTEMS

\[ I_p = 400 \text{ AMPS} \times \frac{2.4\text{KV}}{\sqrt{3} \times 13.8\text{KV}} \]

\[ I_p = 40 \text{ AMPS ON PHASE A & C.} \]
400 AMP GROUNDING

Disadvantages
• Relatively large ground fault is required and thermal damage and core restacking is possible
• The faulted machine is shutdown
• Starter fuse may also operate
• Must trip upstream circuit breaker.

Advantages
• 400 amp grounding does look at a large part of the machine winding.
HIGH RESISTANCE GROUNDING
OF POWER SYSTEMS
THE HIGH RESISTANCE GROUNDED POWER SYSTEM

SUITABLE FOR
- TWO WIRE, SINGLE PHASE LOADS
- THREE WIRE, THREE PHASE LOADS

NOT SUITABLE FOR
- TWO WIRE, LINE TO NEUTRAL LOADS
No Single Phase Loads

No line-to-neutral loads allowed, prevents Hazards.

Line-to-neutral Voltage is backfed via neutral wire, thus, not allowed.

Ground ≈ AØ
HIGH RESISTANCE GROUNDING
EXAMPLE

2000KVA, 480 VOLT SYSTEM

RESISTOR 55.40HMS

Ica=1.0A  Icc=1.0A  Icb=1.0A

Xco  Xco  Xco

Ig = 0

LET Xco BE 277 OHMS (TYPICAL)
HIGH RESISTANCE GROUNDING – GROUND FAULT ON PHASE A
HIGH RESISTANCE GROUNDING – GROUND FAULT ON PHASE A

\[ V_b \]  
\[ V_C \]  
\[ 55.4 \text{ohm resistor} \]

\[ I_{cc} = (1.0 \text{Amp} \times \sqrt{3}) = 1.73 \text{A} \]

\[ I_g = 3I_{cc} = 3.0 \text{A} \]

\[ I_{g} = 3I_D = 3.0 \text{A} \]

\[ 1.73 = I_{cc} \]

\[ 1.73 = I_{cb} \]

\[ 5.83 \text{A} \]

\[ I_R = 5 \text{A} \]

\[ I_g = \sqrt{(5)^2 + (3.0)^2} = 5.83 \text{Amps} \]
HIGH RESISTANCE GROUNDED SYSTEM
LINE-GROUND SHORT CIRCUIT

TRANSFORMER TURNS RATIO = \( \frac{13,800 \text{ VOLTS}}{(480/\sqrt{3}) \text{ VOLTS}} = 49.79 \)

\[ l_0 = \frac{5A}{49.79} = 0.1 \text{ AMP} \]

THUS, UNLIKE THE SOLIDLY GROUNDED SYSTEM, THE HIGH RESISTANCE GROUNDED SYSTEM CREATES NO PROBLEMS ON THE PRIMARY SYSTEM.
THE HIGH RESISTANCE GROUNDED POWER SYSTEM
CONTROL OF TRANSIENT OVERVOLTAGE

\[
\frac{\text{Resistor KW}}{\text{Charging KVA}} = \frac{Ir}{3\text{ICD}}
\]

Ref. Westinghouse Transmission & Distribution Reference Book p. 521
How Modern High Resistance Grounding Systems Calculate the Capacitive Charging Current

\[ I_c = \sqrt{I_f^2 - I_r^2} \]

\[ I_f = I_r + 3I_{co} \]
HIGH RESISTANCE GROUNDING OF A 2400 / 1385 VOLT SYSTEM
THE HIGH RESISTANCE GROUNDED POWER SYSTEM
CHOOSING THE GROUND RESISTOR

Always specify a continuously rated resistor for 5 amps for all system voltages.

<table>
<thead>
<tr>
<th>SYSTEM VOLTAGE</th>
<th>RESISTOR AMPS</th>
<th>RESISTOR OHMS</th>
<th>RESISTOR WATTS (CONTINUOUS)</th>
</tr>
</thead>
<tbody>
<tr>
<td>380</td>
<td>5</td>
<td>43.88</td>
<td>1,097</td>
</tr>
<tr>
<td>415</td>
<td>5</td>
<td>47.92</td>
<td>1,198</td>
</tr>
<tr>
<td>480</td>
<td>5</td>
<td>55.4</td>
<td>1,385</td>
</tr>
<tr>
<td>600</td>
<td>5</td>
<td>69.3</td>
<td>1732</td>
</tr>
<tr>
<td>2400</td>
<td>5</td>
<td>277</td>
<td>6,925</td>
</tr>
<tr>
<td>3300</td>
<td>5</td>
<td>295</td>
<td>7,375</td>
</tr>
<tr>
<td>4160</td>
<td>5</td>
<td>480</td>
<td>12,000</td>
</tr>
</tbody>
</table>
ADVANTAGES
1. Low value of fault current
2. No flash hazard
3. Controls transient over voltage
4. No equipment damage
5. Service continuity
6. No impact on primary system
7. Easily find Grounds on the system
HOW DO YOU FIND GROUND FAULTS?

Ungrounded
Solidly grounded
Low resistance grounded
High resistance grounded
PROCEDURE FOR LOCATING GROUND FAULT

1. Alarm indicates ground fault.

2. Technician confirms ground faults by visiting substation.

3. Voltage on meter relay

4. Current through ground resistor.

5. Substation zero sequence feeder ammeters will indicate specific feeder to MCC or Power Distribution Panel.

6. Go to specific MCC or PDP, open wireway and use clamp-on ammeter around outgoing leads to determine failed circuit.

7. Evaluate need to replace or fix component.
Ground Fault Location Method

NOTE: Tracking a ground fault can only be done on an energized system. Due to the inherent risk of electrocution this should only be performed by trained and competent personnel wearing proper PPE clothing.
Fault Location

Method to quickly locate ground faults.

Meter reading will alternate from 5A to 10A every 2 seconds.
The reasons for limiting the current by resistance grounding may be one or more of the following.

1) To reduce burning and melting effects in faulted electric equipment, such as switchgear, transformers, cables, and rotating machines.

2) To reduce mechanical stresses in circuits and apparatus carrying fault currents.

3) To reduce electric-shock hazards to personnel caused by stray ground-fault currents in the ground return path.
Per IEEE…

TO HRG OR NOT TO HRG?

IEEE Std 142-1991 (Green Book)
Recommended Practice for Grounding of Industrial and Commercial Power Systems

1.4.3  The reasons for limiting the current by resistance grounding may be one or more of the following.

4)  To reduce the arc blast or flash hazard to personnel who may have accidentally caused or who happen to be in close proximity to the ground fault.

5)  To reduce the momentary line-voltage dip occasioned by the clearing of a ground fault.

6)  To secure control of transient over-voltages while at the same time avoiding the shutdown of a faulty circuit on the occurrence of the first ground fault (high resistance grounding).
IEEE Std 141-1993 (Red Book)
Recommended Practice for Electric Power Distribution for Industrial Plants

7.2.2  *There is no arc flash hazard, as there is with solidly grounded systems, since the fault current is limited to approximately 5A.*

*Another benefit of high-resistance grounded systems is the limitation of ground fault current to prevent damage to equipment.* High values of ground faults on solidly grounded systems can destroy the magnetic core of rotating machinery.
IEEE Std 242-2001 (Buff Book)
Recommended Practice for Electric Power Distribution for Industrial Plants

8.2.5 Once the system is high-resistance grounded, over-voltages are reduced; and modern, highly sensitive ground-fault protective equipment can identify the faulted feeder on the first fault and open one or both feeders on the second fault before arcing burn down does serious damage.
Design Considerations with HRG Systems

National Electrical Code (2005)

250.36 High-impedance grounded neutral systems in which a grounding impedance, usually a resistor, limits the ground-fault current to a low value shall be permitted for 3-phase ac systems of 480 volts to 1000 volts where all the following conditions are met:

1) The conditions of maintenance and supervision ensure that only qualified persons service the installation.
2) Continuity of power is required.
3) Ground detectors are installed on the system.
4) Line-to-neutral loads are not served.
# Duty Ratings for NGR’s

IEEE Std 32

Time Rating and Permissible Temperature Rise for Neutral Grounding Resistors

<table>
<thead>
<tr>
<th>Time Rating (On Time)</th>
<th>Temp Rise (deg C)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ten Seconds (Short Time)</td>
<td>760°C</td>
</tr>
<tr>
<td>One Minute (Short Time)</td>
<td>760°C</td>
</tr>
<tr>
<td>Ten Minutes (Short Time)</td>
<td>610°C</td>
</tr>
<tr>
<td>Extended Time</td>
<td>610°C</td>
</tr>
<tr>
<td>Continuous</td>
<td>385°C</td>
</tr>
</tbody>
</table>

*Increased Fault Time Requires Larger Resistor*

*Duration Must Be Coordinated With Protective Relay Scheme*
COMPARISON OF THE FOUR METHODS
# HIGH RESISTANCE GROUNDING OF A 2400 VOLT MOTOR SYSTEM

## COMPARISON OF SOME CHARACTERISTICS

<table>
<thead>
<tr>
<th>CHARACTERISTIC</th>
<th>UNGROUNDED</th>
<th>HIGH R. GROUNDING</th>
<th>LOW R. (&lt;400A) GROUNDING</th>
<th>EFFECTIVE GROUNDING</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. CURRENT FOR A PHASE-GROUND FAULT AS A PERCENTAGE OF 3Ø FAULT CURRENT</td>
<td>LESS THAN .05%</td>
<td>~ 5%</td>
<td>~ 100%</td>
<td></td>
</tr>
<tr>
<td>2. TRANSIENT OVERVOLTAGE</td>
<td>UP TO 6X</td>
<td>MAX OF 2.5 TIMES</td>
<td></td>
<td></td>
</tr>
<tr>
<td>3. AUTO FAULT LOCATION</td>
<td>NO</td>
<td>YES</td>
<td></td>
<td></td>
</tr>
<tr>
<td>4. IMMEDIATE DISCONNECTION OF PHASE-GROUND FAULT</td>
<td>NO</td>
<td>OPTIONAL</td>
<td>NECESSARY</td>
<td></td>
</tr>
<tr>
<td>5. EXPECTED REPAIRS AFTER AN INITIAL PHASE-GROUND FAULT IN A MOTOR</td>
<td>&lt;NEW WINDING INSULATION&gt;</td>
<td>PROBABLY CORE RESTACKING</td>
<td>CORE RESTACKING</td>
<td></td>
</tr>
<tr>
<td>6. MULTIPLE FAULTS</td>
<td>OFTEN</td>
<td>Seldom</td>
<td></td>
<td></td>
</tr>
<tr>
<td>7. 1^2t DAMAGE</td>
<td>LOW</td>
<td>HIGH</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
THE HIGH RESISTANCE GROUNDED POWER SYSTEM

DAMAGE TO POWER SYSTEM COMPONENTS

1. Thermal damage

\[ (I_{RMS})^2 t \]

2. Mechanical damage

\[ (I_p)^2 \]

Comparison of solidly grounded and high resistance grounding methods – 2000 KVA transformer at 480 volts

<table>
<thead>
<tr>
<th>SYSTEM GROUNDING</th>
<th>LINE-GROUND FAULT AMPS</th>
<th>DAMAGE TO EQUIPMENT</th>
</tr>
</thead>
<tbody>
<tr>
<td>Hi – R</td>
<td>5 A</td>
<td>1 per unit</td>
</tr>
<tr>
<td>Solidly</td>
<td>20,000 A</td>
<td>16 x 10^6</td>
</tr>
</tbody>
</table>

Increase in damage = \( \left( \frac{20,000 \text{ A}}{5 \text{ A}} \right)^2 = 16,000,000 \)
THE HIGH RESISTANCE GROUNDING
OF POWER SYSTEM

The high resistance grounded power system provides the following advantages:

1. No shutdowns when a ground fault occurs
2. Quick identification of the problem
3. Safer for personnel & equipment
4. Offers all of advantages of the ungrounded & solidly grounded systems
5. No known disadvantages
Should High Resistance Grounding be used to help prevent Arc Flash Hazards to Personnel?
Absolutely!! Since 98% of faults start off as a phase to ground faults, this will lower the current that is supplied to the fault.
Can I lower the Amps Interrupting Capacity (AIC) rating of my switchgear, if I have a neutral grounding resistor?
No. You could still have a phase to phase fault that could produce the high current fault levels.
Retrofit from Solidly or Ungrounded Grounded System to High Resistance Design Considerations

1. Are cables rated line to line or line to neutral. On a 480 Volt system some people have installed 300 Volt cable.

2. Are there surge arrestors and MOV’s on the system. Are they sufficiently rated?

3. Are the Neutrals on the transformers fully insulated?

4. Are there other sources of power on the circuit? Generators or Tie Breakers
Resolve NEC requirement

Add small 1:1 transformer and solidly ground secondary for 1Φ loads (i.e. lighting).
High Resistance Grounding

What if no neutral exists (i.e. delta systems)?

– A grounding transformer is installed (either a zig-zag or a wye-delta) from all three phases to create an artificial neutral for grounding purposes only.
Zig-Zag Wiring
Minimum Specifications

120 Volt Control Circuit
385°C Temperature Rise Resistor
Line Disconnect Switch
Ground Bus (freestanding units only)
Pulser, Including Pulsing Contractor, Pulsing Timer, Normal/Pulse Selector Switch
Relays for under and over voltage
Relays for under and over current measuring only fundamental
Auxiliary contacts
Test Push-button
Fault Reset Push-button
Green Indicating Light for “Normal” Indication
Red Indicating Light for “Fault” Indication
CHARGING CURRENT CALCULATIONS

Some manufactures are now bringing in the 3 phase voltages and determining the capacitive charging current on the actual system.

Slides to Calculate are hidden due to time allowed for Presentation
GENERATOR APPLICATIONS
OF NEUTRAL GROUNDING RESISTORS
GENERATOR APPLICATIONS OF NEUTRAL GROUNDING RESISTORS

1. All generators should use a NGR.
2. If you have 2 generators on a system with different pitches you will need to use 2 NGRs to limit the harmonics that are generated.
3. On a delta generator you should use an NGR with a zig-zag transformer.
IEEE Std 242-2001 (Buff Book)
12.4 Generator Grounding

- **A common practice is to ground all types of generators through some form of external impedance.** The purpose of this grounding is to limit the mechanical stresses and fault damage in the machine, to limit transient voltages during fault, and to provide a means for detecting ground faults within the machine…

Solid grounding of a generator neutral is not generally used because this practice can result in high mechanical stresses and excessive fault damage in the machine…

Generators are not often operated ungrounded. While this approach greatly limits damage to the machine, it can produce high transient overvoltages during faults and also makes it difficult to locate the fault.
1.8.1 Discussion of Generator Characteristics

• Unlike the transformer, the three sequence reactances of a generator are not equal. The zero-sequence reactance has the lowest value, and the positive sequence reactance varies as a function of time. **Thus, a generator will usually have higher initial ground-fault current than a three-phase fault current if the generator is solidly grounded. According to NEMA, the generator is required to withstand only the three-phase current level unless it is otherwise specified**…

A generator can develop a significant third-harmonic voltage when loaded. A solidly grounded neutral and lack of external impedance to third harmonic current will allow flow of this third-harmonic current, whose value may approach rated current. If the winding is designed with a two-thirds pitch, this third-harmonic voltage will be suppressed but zero-sequence impedance will be lowered, increasing the ground-fault current…

**Internal ground faults in solidly grounded generators can produce large fault currents.** These currents can damage the laminated core, adding significantly to the time and cost of repair…Both magnitude and duration of these currents should be limited whenever possible.
AIC Rating
*(Amps Interrupting Current)*

This example is taken from lowzero.pdf by Power Systems Engineering

- 3 Phase Short Circuit Calculations for the Generator is 11.1 kA
- Line to Ground Fault Current for the Generator is 13.8 kA because the zero sequence impedance ($X_0$) is lower than the positive sequence impedance ($X_1$)

Line to Ground Fault Current is 125% of the Phase Current Fault in this example

Solution – Make sure you check your AIC rating of the equipment and use a Neutral Grounding Resistor.
A large generator (≥ 20 MVA, 13,800 volt) may take 5 to 20 seconds to stop. A IEEE working group wrote a series of four papers. They proposed a hybrid system having a low resistance grounding system and when the fault occurred switch to a high resistance grounded system.
HYBRID SYSTEM

13,800 Volt 40 MVA Generator

Contact Closed in normal operation

High Resistance NGR

Low Resistance NGR
Pictures of Equipment
Common options

- Enclosure rating
- Enclosure finish
- Current transformer
- Potential transformer
- Disconnect switch
- Entrance/exit bushings
- Elevating stand
- Seismic rating
- Hazardous area classification
- Third party certification
IEEE | Edit

Here are links to presentations and information that has been given by Levine Lectronics and Lectric at IEEE Meetings.

ANSI Symbols

ANSI-GT-C37-2 Paper

Conversion of Electromechanical settings to Digital settings

EASA Root Cause Failures

GE Digital Relays 2010

IEEE Communications-2010

IEEE CTs and PTs 2011

IEEE Generator Protection

IEEE Hybrid Grounding

Low Zero-Sequence Impedances on Generators

Motor Protective Settings

Post Glover Resistance Grounding 2011

Protection Relay Basics

PSRC CT Saturation Calculator

Manufacturers

AC Tech

Airotronics

Alstom Grid

Attaxo

Dynapar-Northstar-Lakeshore

GE Breaker Retrofit Kits

GE ITI

GE Monitoring and Diagnostics

GE Multilin

Kinney Electrical

Micron Industries Corporation

Pacific Crest Transformers

Post Glover Resistors

Sky-Young Electronics

Spracher + Schuh

Visual and Listed Line Card

Line Card

Visual Line Card
Thank You

Questions?